



Robust Autonomous Aerobraking Strategies

9th International Planetary Probe Workshop

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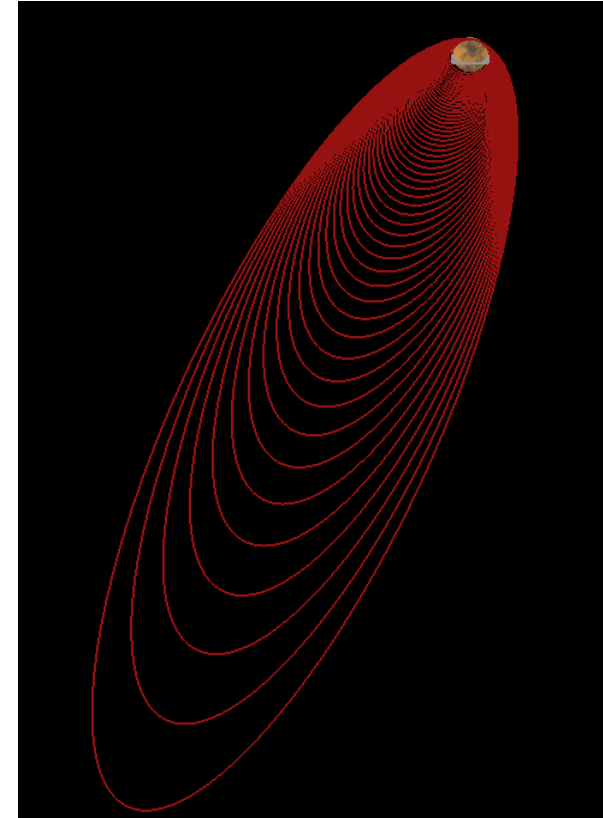


Outline

- Introduction & mission scenario
- High-fidelity aerobraking simulator (HiFAS)
- AOCS for aerobraking
- Autonomous aerobraking: level 1 & level 2
- Safe mode for aerobraking
- Conclusions and future work

Introduction

- Aerobraking consists in using atmospheric air drag in order to reduce the orbit's apoapsis altitude
 - Allows significant mass savings with direct benefits to mission design
 - Aerobraking has been performed on several US missions to Venus and Mars, and an European experiment is planned in 2014 on VEX
 - Baselined on recent ESA system studies (MarsNEXT, MSR Orbiter)
- However, aerobraking remains a challenging phase:
 - High cost due to ground operations heavy workload
 - Risk of spacecraft component over-heating, or even mission loss
- The main objective of the study is to define and select aerobraking strategies aiming at:
 - Gradually increasing aerobraking autonomy level
 - Guaranteeing aerobraking robustness
- Performed in the frame of ESA study "Robust Autonomous Aerobraking Strategies"



Aerobraking mission scenario

- ESA MarsGen is to be used as reference mission

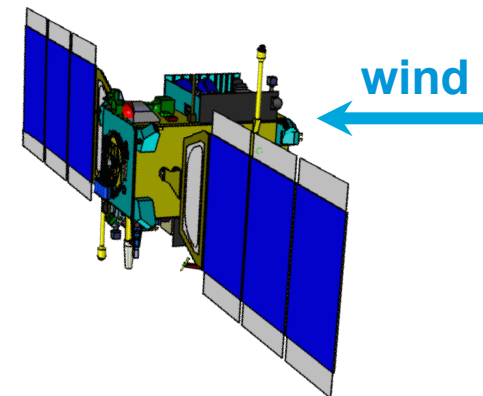
- ESA system study performed in 2009
- Mars network science mission (launch 2020 – 2022)
- Follow-up study to MarsNEXT

- The selection of the aerobraking scenario is the result of a trade-off between:

- Spacecraft characteristics
- Propellant consumption
- Aerobraking aggressiveness
- Aerobraking duration

- The resulting operational point is as follows:

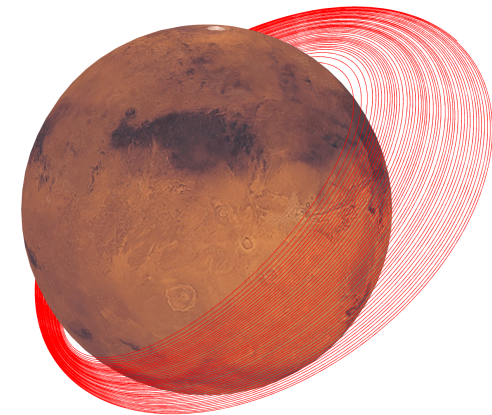
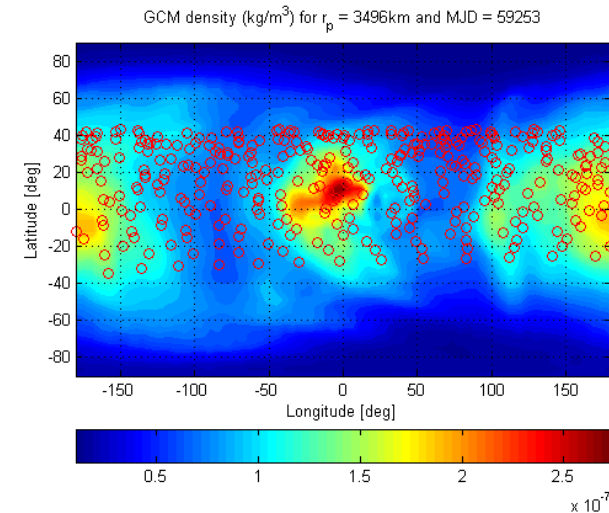
- Ballistic coefficient of 25 kg/m²
- Initial apoapsis altitude at 67500km
- Peak dynamic pressure at 0.5 N/m²
- These conditions allow limiting the duration of aerobraking to 6 months (including margins)



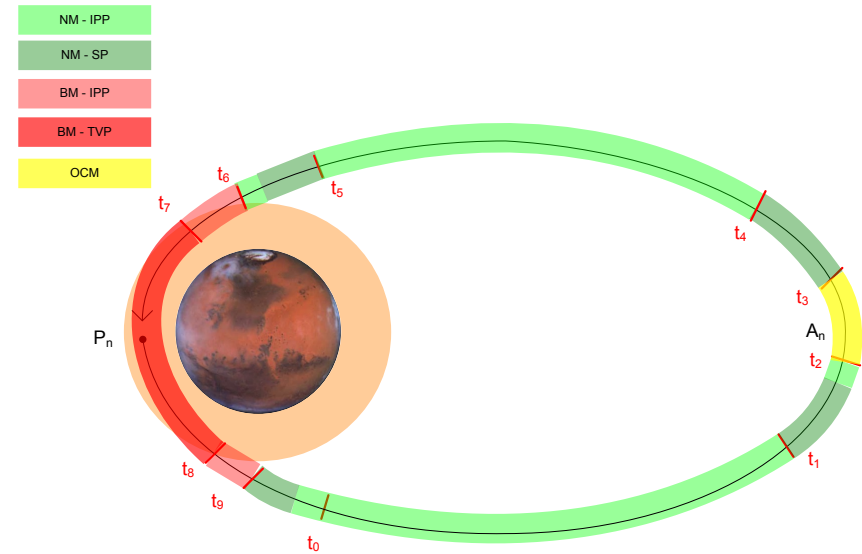
| B [kg/sqm] | p-peak [N/sqm] | q-peak [W/sqm] | Phase dur. [d] | Init. apocentre alt. [km] | Apocentre lowering man. [m/s] | Pericentre control [m/s] | Apocentre raising [m/s] |
|------------|----------------|----------------|----------------|---------------------------|-------------------------------|--------------------------|-------------------------|
| | 0.3 | 1350 | 150 | 35000 | 132 | 22 | 99 |
| 25 | 0.5 | 2250 | 150 | 67500 | 34 | 14 | 100 |
| | 0.7 | 3200 | 140 | 96000 | 0 | 11 | 101 |
| 35 | 0.3 | 1300 | 150 | 23500 | 217 | 31 | 99 |
| | 0.5 | 2200 | 150 | 43000 | 96 | 20 | 100 |
| | 0.7 | 3200 | 150 | 67000 | 35 | 14 | 101 |
| 50 | 0.3 | 1280 | 150 | 16000 | 321 | 39 | 99 |
| | 0.5 | 2200 | 150 | 28000 | 177 | 27 | 100 |
| | 0.7 | 3150 | 150 | 41500 | 102 | 21 | 101 |

High-fidelity Aerobraking Simulator (HiFAS)

- Main objective is to implement, validate and evaluate autonomous aerobraking strategies
- Environment modelling is critical in order to properly capture the effects that drive the aerobraking phase
 - Mars atmosphere density variations
 - ➔ high-fidelity Mars atmosphere models including both short-scale and long-scale perturbations: Mars Climate Database, General Circulation Model
 - Aerobraking orbit evolution
 - ➔ 20x20 Mars gravity field and Solar gravity
 - Temperatures of critical elements
 - ➔ S/C thermal model, for both MLI and solar arrays
 - Power status (e.g. for safe mode validation)
 - ➔ S/C battery charge model
- Management of different regimes (drag/vacuum)
 - Implementation of a « variable scheduler » in order to manage different simulation time steps and minimize computation time
 - Enables simulations from one atmospheric pass (~1000s) up to typically one week for full « end-to-end » validation

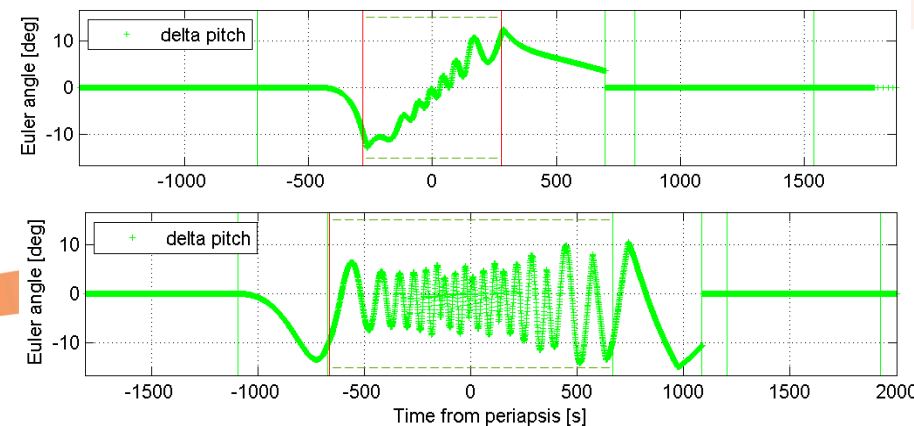
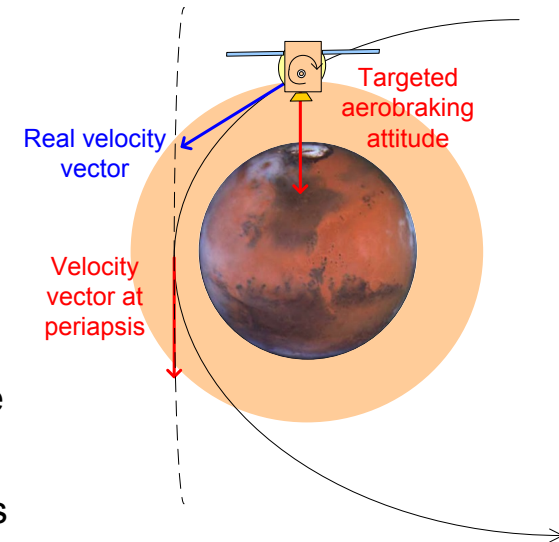


AOCS for aerobraking: AOCS modes and sequences



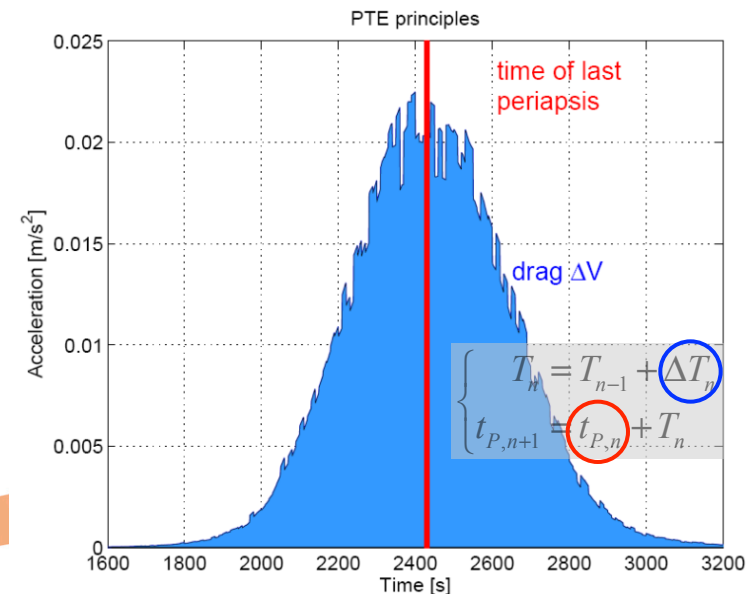
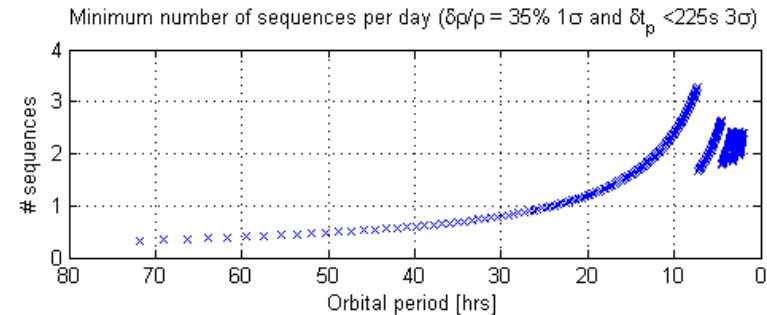
AOCS for aerobraking: AOCS design

- Attitude control is based on an aerodynamically stable S/C configuration
 - Avoid fighting the aerodynamic torque
 - Wide deadband, thruster-based control as safeguard
- Guidance is inertial until final stage of aerobraking, then time-varying as the orbit becomes circular
 - Time-varying guidance generates timing constraints, since the attitude profile must be close enough to the actual velocity vector
 - For instance, a 15 deg maximum attitude error leads to a 180s periapsis timing error in the end of aerobraking (worst case)
 - In the case of inertial pointing, this timing constraint is relaxed
- The proposed AOCS baseline is validated by simulations
 - Attitude is always kept within ± 15 deg around guidance profile
 - Consumption remains reasonable (a few grams per pass)
 - Validity of inertial guidance in the beginning of aerobraking is confirmed



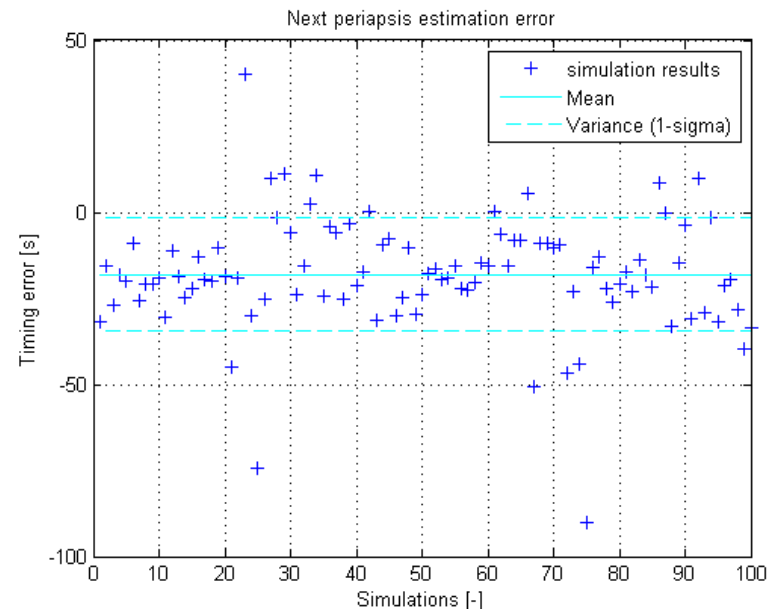
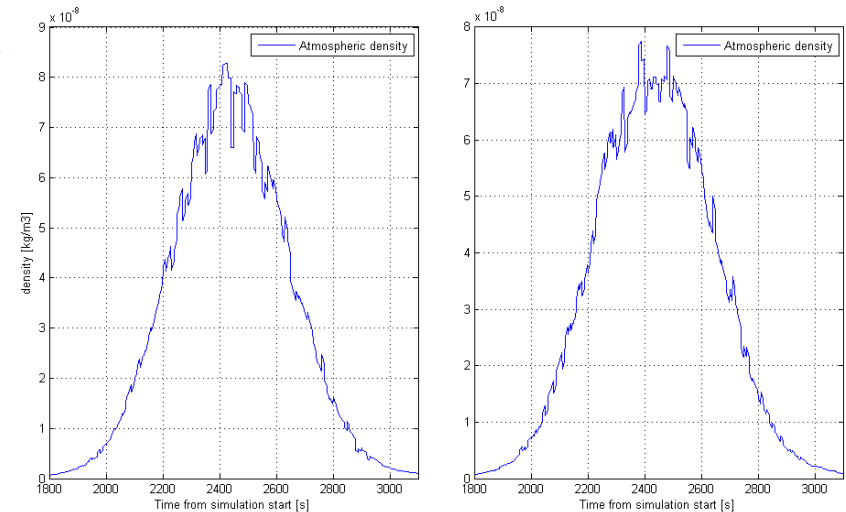
Autonomy level 1: Motivation and design

- Because of atmospheric variability and misknowledge, AOCS sequences generated by the ground are quickly out-of-sync with actual orbit events
 - May lead to extra-propellant usage or unsafe situations
 - Heavy operational workload in order to ensure proper timing
 - But orbit timing may be detected autonomously via onboard accelerometers
- Objectives of autonomy level 1:
 - Shift upcoming drag sequences in time in order to match actual orbit events, based on onboard atmospheric sensing → **Periapsis Time Estimator**
 - Protect the spacecraft against excessive heat loads not foreseen by ground → **Immediate Action procedure**
- Principles of the Periapsis Time Estimator:
 - Firstly, the time of last periapsis is estimated from drag barycenter
 - Then accumulated drag ΔV is used to update orbital period and predict time of next periapsis
 - Thus after each drag pass, the timing of the next orbit is autonomously corrected, without any error growth



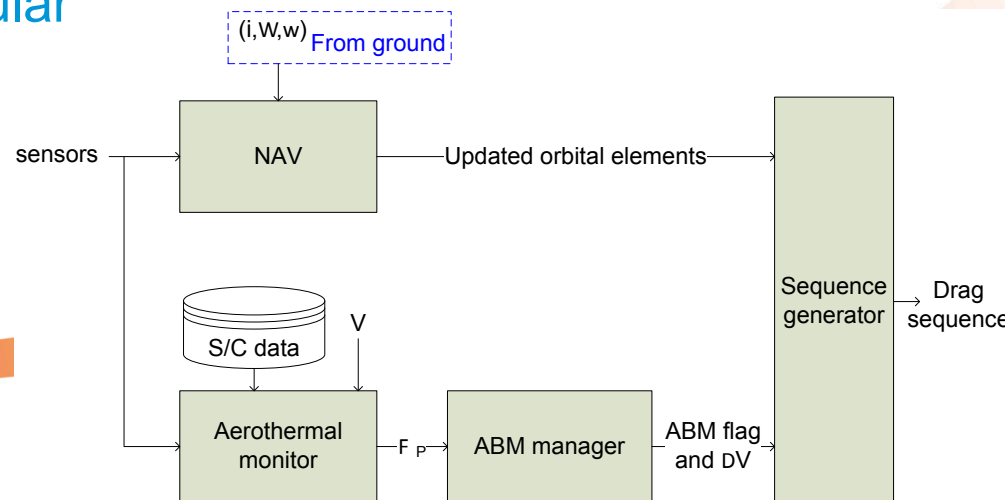
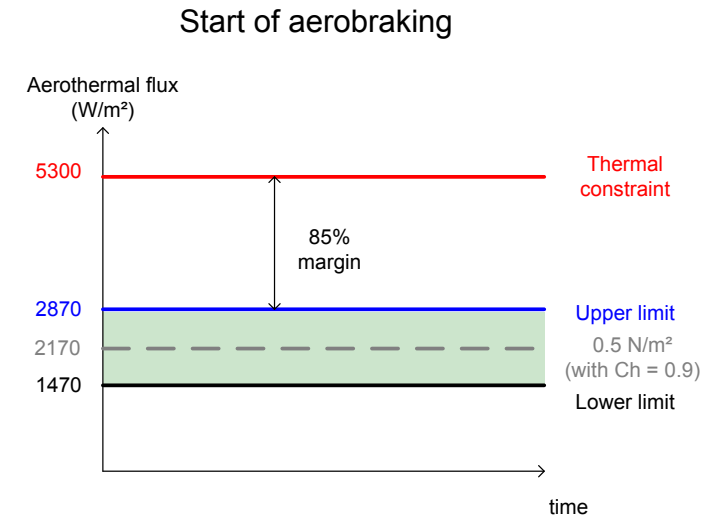
Autonomy level 1: Simulation results and conclusions

- The Periapsis Time Estimator (PTE) was validated on a wide range of conditions
 - Different orbital geometry cases
 - Varying atmospheric conditions, including both long-scale and short-scale atmospheric perturbations
 - Varying sensor noises
- The PTE predicts the time of next periapsis with the required accuracy (< 180s) over 3 days and more
 - Performances improve over aerobraking as sensitivity to drag $\propto V$ estimation error decreases
 - Robustness to atmospheric perturbations has been demonstrated
- Additional lessons learned:
 - The implementation of a corrective factor to account for non-instantaneous drag $\propto V$ is required
 - Calibration of accelerometers bias before each pass is necessary (in the beginning of aerobraking)



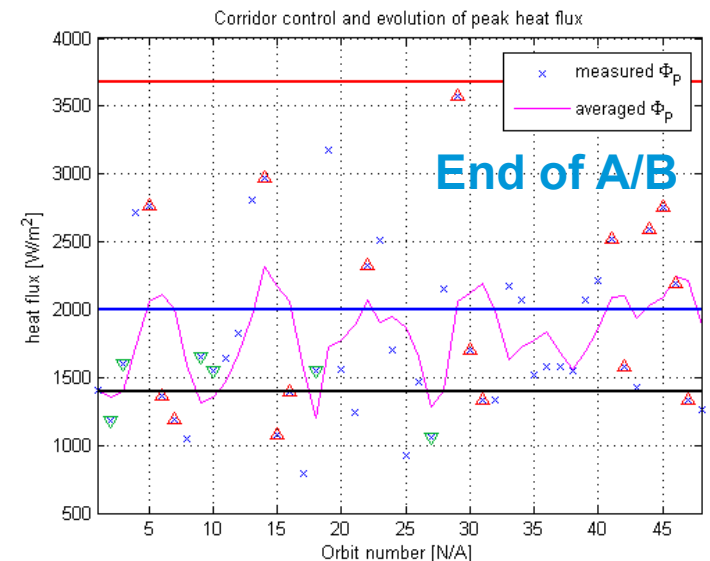
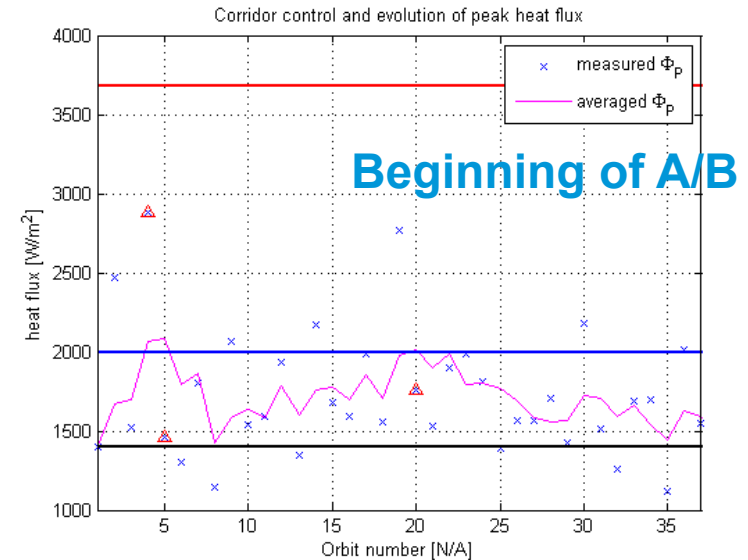
Autonomy level 2: Motivation and design

- Main objective: extend S/C autonomy by transferring additional activities onboard
 - Relieve the ground from most low-level activities, so that it may focus on high-level activities
 - Target autonomy horizon of **one week** for identified activities
- Two activities were considered for onboard implementation:
 - Drag sequences generation
 - Corridor control, i.e. ABM analysis, decision-making and selection
- The ground still performs regular orbit determination and high-level activities, such as:
 - Monitor aerobraking progress
 - Update aerobraking corridor
 - Atmosphere monitoring and trending
 - Modelling updates




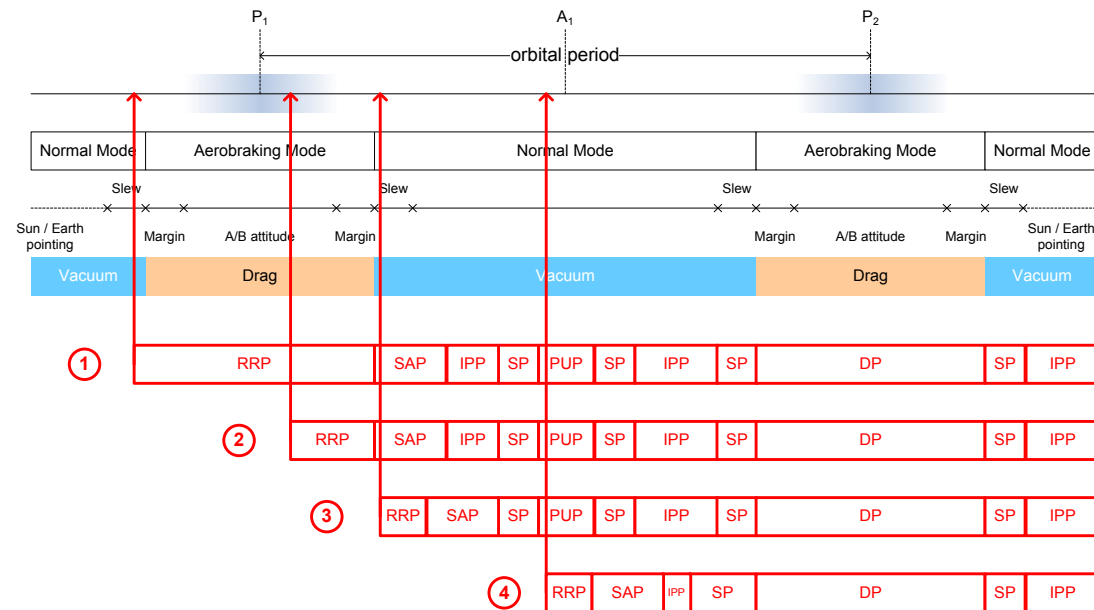
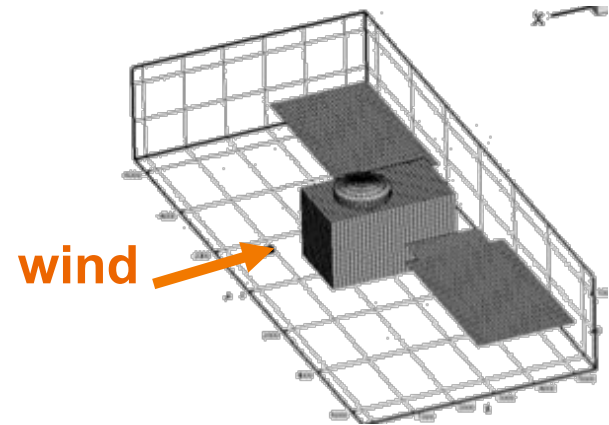
Autonomy level 2: Simulation results and conclusions

- The algorithms of level 2 were implemented and validated over one week, with satisfactory results
 - Almost no excessive heat flux occurrences
 - Achieved dynamic pressure peak is between 0.49 N/m^2 and 0.76 N/m^2 , exceeding the target 0.5 N/m^2
 - Reasonable \mathbb{W} V consumption for corridor control, extrapolated to $\sim 40 \text{ m/s}$ over 6 months in worst case
 - Frequency of the required ground updates to support onboard navigation has been preliminary estimated (from > 7 days to ~ 3 days in the end)
- The simple approach to autonomous corridor control works
 - Minimal onboard navigation, simple heat flux control approach
 - Potentially removes the need for complex onboard propagator, models, fully autonomous navigation



Aerobraking safe mode

- Classical safe mode for interplanetary missions may lead to arbitrary attitude in atmospheric flow → dynamics, thermal, orbital decay issues
- Trade-off between different solutions led to the combination of a low-drag configuration and pop-up  V
- Design validated by simulations, based on thermal, power, orbital decay criteria



- safe mode just before atmospheric entry; not enough time to go to aerobraking configuration
- safe mode during atmospheric pass
- safe mode right after atmospheric pass
- safe mode around apoapsis ; not enough time to perform pop-up boost at apoapsis

Conclusions and future work

- The AOCS design for aerobraking has been validated
- The PTE has been validated, enabling autonomy level 1
- The feasibility of the simple approach to autonomous corridor control has been demonstrated
- The proposed safe mode design has been validated by simulations, ensuring S/C safety
- The immediate action procedure triggered in case of thermal alarm was validated, reducing the experienced temperatures at the next periapsis even in the case of a global dust storm
- Next step: validate and evaluate autonomy algorithms during VEX aerobraking experiment (2014) → first demonstration of their operational capabilities

Thank you for your attention !



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